Contract V81621, West Levee Alignment Study, Craney Island, Norfolk Harbor, Norfolk, Virginia (Contract No. DACW-65-81-D-0020)

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SCHNABEL ENGINEERING ASSOCIATES. P.C.

CONSULTING GEOTECHNICAL ENGINEERS.

January 22, 1982

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Attn: Mr. Jack G. Starr Chief, Engineering Division Contract V81621, West Levee Alignment Study, *Craney Island, Norfolk Harbor, Norfolk, Virginia (Contract No. DACW-65-81-D-0020) Subject:

Gentlemen:

Submitted herewith are four copies of our report for the above relaboratory testing, and engineering analysis made in accordance with our agreement dated December 22, 1981. This report covers the subsurface investigation, ferenced project.

Scope

(A) Subsurface Field Investigation, Our scope of services included: (A) Subsurface Field Investigation (B) Layout and Inspection of Field Investigation, (C) Soil Laboratory Testing, and (D) a Geotechnical Engineering Analysis. The geotechnical engineering analysis included the study of test borings, geological, soil test and groundwater data to develop the following:

- .. An estimated geologic profile along the levee.
- 2. Shear strength parameter recommendations.

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No construction inspection, stability analysis, quantity estimates, or detailed plans and specifications were included in this study.

Conclusions and Recommendations

Based on the information contained in this report, the following summary of conclusions and recommendations is presented: Norfolk District Corps of Engineers January 22, 1982 Page Two

- extends to depths of 23 to 74 ft in the study area and is underlain by a soft, highly plastic marine clay (Stratum B) having low to moderate shear strength. £111
- slightly Similar strength values were obtained for both triaxial testing and vane shear testing within the clay stratum, with vane tests higher as expected. The strength of the clay formation appears increase with depth.
- 3. We believe the shear strength of the marine clay can best be characterized by utilizing an undrained strength of 350 to 400 psf above El -65, and a value of 550 to 600 psf below this elevation.

Site Description, Proposed Construction and General Subsurface Conditions

the disposal area could potentially be raised to increase the life expectancy of this site. The purpose of this study is to determine subsurface conditions and perform laboratory testing to provide appropriate strength data so that a stability analysis may be performed for the raised The field investigation and laboratory test program were developed Craney Island is a slurry disposal area for the U. S. Army Corps of Engineers dredging operations in the vicinity of the Norfolk Harbor. This disposal area is ringed by a levee approximately 15 to 25 feet above sea level, which is gradually becoming filled. The levee surrounding by your office.

Seven test borings were drilled by Ayers and Ayers, Inc., Richmond, Virginia, under our inspection in December, 1981 and January, 1982. Test boring logs are included in Enclosure 2 with test boring locations shown . An estimated subsurface profile, Sheet 2, is also included in the enclosure. The test borings indicate the following generalized soil strata underlie the site to the depths investigated: on Sheet 1

Stratum A: From ground surface to depths of 23 to 74 ft

Tan, brown or gray fine to coarse sand FILL with variable amounts of silt and clay (SP, SM and SC); very loose to very compact density (N = 3 to 50)

Stratum B: Below Stratum A to maximum depth of penetration, 115 ft

Gray, CLAY, trace fine sand with shell fragments (CH); soft consistency (N = WOR to 8)

Stratum C: Below Stratum B to maximum depth of 113 ft in Boring DH-7

Dark gray fine sandy CLAY with wood fragments (CL); soft to medium consistency (N = WOR to 6); and gray fine to medium SAND, trace clay (SC); very loose density (N = WOR)

Norfolk District Corps of Engineers January 22, 1982 Page Three Stratum D: Below Stratum C in Boring
DH-7 to the maximum depth
of penetration 115 ft

Gray-green fine to medium SAND, trace silt (SM); compact density (N = 45)

spoon one foot using a 140 pound harmer falling 30 inches. This test is conducted after seating the sampler six inches in the bottom of the hole according to ASTM D-1586. resistances encountered in a particular layer as determined from the number of blows required to drive a 2 inch 0.D., 1-3/8 inch I.D. sampling The above N values indicate the low and high Standard Penetration Test

to be natural This material was probably brought to the site from local borrow Stratum A soils are a sandy fill with variable amounts of silt and areas to build the existing levee. Stratum B soils appear to be naturarine and estuarine clays deposited by the lower James and Nansemond River Systems at Hampton Roads.

Stratum C soils represent transition clays and sands between the Stratum D marine clays and the Miocene age, Yorktown Formation. Strat soils are probably the upper part of the Yorktown Formation. Groundwater was encountered at depths of 5 to 7 feet in all borings, Long-term water level corresponding to elevations of +2 to sea level. Long-term water leveradings indicated all borings dry at the shallower cave depths of 1.2 to 4.5 ft. Recorded groundwater levels appear to reflect the phreatic surface within the levee embankment,

Laboratory and In situ Testing

Tests of Enclosure Twelve undisturbed tube samples were tested in our soils laboratory n results included in the Summary of Soil Laboratory Tests of Enc Classifications are in accordance with the Unified Soils System, ASTM D-2487.

Brown fine to coarse sand with clay layers and shell fragments (SP) Stratum A:

layers. Only about 5% material by weight within the sandier zones passed the No. 200 sieve. These soils should be considered as poorly graded due to dry density of 95 pcf was measured at a natural moisture content of 22.3%. The Plasticity Index was 36 indicating moderate plasticity for the clay A fairly high natural One tube sample was obtained within Stratum A. the clay layers present.

Dark gray fine sandy clay with wood fragments (CL) Stratum C:

One vane shear test was performed within this stratum. The undrained vane shear strength was found to be S_{ij} = 3450 psf as shown in Enclosure 1. This value is much higher than those encountered in Stratum B, most likely due to the increased sand content in this stratum.

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Stratum B: Gray clay, trace fine sand (CH)

Natural density and moisture was measured for each sample within this unit. The natural dry densities were low ranging from 51 to 66 pcf. Natural moisture contents often approached liquid limit values indicating a relatively soft material. Values of 43 to 82% were recorded. The Plasticity Index varied from 34 to 68, indicating moderate to high plasticity as expected for this material. A maximum of only 5% material by weight was retained on the No. 200 sieve, indicating predominately fine-grained material. Liquidity Indices were found to range from 0.19 to 1.12. Based on the high average value of 0.82 and sensitivity of the material it is estimated that this formation is normally consolidated.

Triaxial test curves are presented in Enclosure 1. These tests were performed in general accordance with ASTM D-2850. Sample diameters were Eleven unconsolidated undrained (UU) triaxial tests were performed. was about approximately 2.8 inches for all test specimens except DH-2/89' and DH-6/34' which had an approximate diameter of 1.9 inches. All test specimens had height to diameter ratios of 2 to 3. All tests except DH-2/89' were performed at about 0.05 in/min corresponding to a strain rate of about 18/min. The strain rate for DH-2/89' was about 0.8%/min, Confining pressures were determined based on approximate effective overburden pressures calculated from laboratory and test boring data.

The following is a summary of undrained shear strengths obtained during this investigation:

| Apparent Cohesion, c | 710 psf | 570 psf | 390 psf | | 740 psf | 120 psf | 310 psf | | 430 psf | 550 psf | 420 psf |
|----------------------|------------|-------------|-------------|-------------|-------------|------------|------------|------------|------------|------------|--------------|
| Boring/Depth | DH-2/71-73 | DH-2/89-91' | DH-3/44-46' | DH-3/64-661 | DH-3/84-861 | DH-5/44-46 | DH-5/69-71 | DH-5/84-86 | DH-6/34-36 | DH-6/79-81 | DH-6/99-101' |

The undrained shear strength typically tends The average As indicated above, values of 120 to 740 psf were obtained. value is about c = 490 psf. to increase with depth.

These tests were performed in accordance with the suggested Sprague & Herwood Vane Test Procedure using a 2" (5.08 cm) vane with an area ratio of 13.4%. Strain rates varied from about 1 to 1.5 degrees per minute. The following is a surmary of the undisturbed undrained shear strength as measured by Eight vane shear tests were also performed in Stratum B as indicated Vane shear tests are shown plotted in Enclosure 1 on the boring logs. this procedure:

| | Undrained Vane Shear |
|--------------|----------------------|
| Boring/Depth | Strength (psf) |
| | |
| DH-1/76-781 | $S_{11} = 2000$ |
| DH-1/84-86' | 11 |
| DH-1/94-961 | 11 |
| DH-4/34-36' | II |
| DH-4/59-61' | II |
| DH-4/84-861 | $S_{11} = 750$ |
| DH-7/44-461 | 11 |
| 17-69/7-HI | 11 |

from the ratio of undisturbed to remolded strengths. The sensitivity of the Stratum B clays ranged from 1.3 to 2.4. These values are relatively low for clays of this plasticity. value is about 935 psf. Remolded strengths varied from 190 to 1000 psf with an average value of about 535 psf. Sensitivity was calculated from As indicated above values of 450 to 2000 psf were obtained.

Evaluation of Results

indicates high strength. Utilizing both laboratory results and corrected field vane results we believe the Stratum B clays can best be characterized by using an undrained strength of 350 to 400 psf above El -65 and 550 to corresponding triaxial test values except in DH-1 where vane shear testing and for Stratum B soils may be taken as 0.8. Utilizing this correction factor the vane shear strength parameters are very close to the those obtained by triaxial testing. The vane shear strengths may be related to the triaxial shear strengths using a correction factor after As expected, values obtained from vane tests were slightly above se obtained by triaxial testing. The vane shear strengths may be This factor is based on the Plasticity Index of the clay, and for Stratum B soils may be taken as 0.8. 600 psf below this elevation. Bjernm.

General

geotechnical engineering practice and make no other warranties, either expressed or implied, as to the professional advice provided under the We have prepared this report in accordance with generally accepted terms of this agreement and included in this report. Norfolk District Corps of Engineers January 22, 1982 Page Six and will then be Soil samples will be held until March 1, 1982, disposed of unless further disposition is requested We appreciate the opportunity to be of service for this project. Please do not hesitate to contact us if clarification is needed for any aspect of this report.

Very truly yours,

SCHAPBEL ENGINEERING ASSOCIATES, P.C.

Bu M Sand

Ann M. Samford Senior Staff Engineer Raymond A. DeStephen, P.E. Commonwealth of Virginia

AMS:RAD:maj

Enclosures

- (1) Summary of Soil Laboratory Tests
 Triaxial Compression Test Curves (11)
 Field Vane Shear Test Curves (8)
- (2) Subsurface Exploration Data
 General Notes for Test Boring Logs
 Identification of Soil Samples
 Test Boring Logs, DH-1 through DH-7
 Test Boring Location Plan, Sheet 1
 Estimated Subsurface Profile, Sheet 2

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SUMMARY OF SOIL LABORATORY TESTS

| See Triaxial Test Curve | 27.2 | 66 | 1 SL | · £₺ | 62 | 7.5 | 99 | 96 | а | Clay-gray (CH) | PduT | 98- | £-на |
|----------------------------|----------------------|------------------------------|----------------------------|---------|--------------------|-----|-------------------------------------|-----|---------|--|--------|----------------------|---------------|
| See Triaxial Test Curve | 89.2 | 00Т | ₽°E9 | 75 | 32 | 69 | Т9 | 00T | Ħ | Clay - gray (CH) | Tube | -83 -16-68 | DH-2 |
| See Triaxial Test | 29.2 | 66 | ۲.42 | 68 | 52 | 19 | 99 | T05 | В | Clay, with shell fragments- gray (CH) | 9dt/T | 99- 121-121 | DH-S |
| | ₽ 7. 2 | S | 22.3 | 98 | 9T | 52 | 96 | 977 | v (as | Tragments-brown(s sand with clay frine to coarse | Tube | <u>96-</u> 164-Th | S-Ha |
| CMLVe See Vane Shear | - | - | - | - | - | 1 | - | - | В | Clay, trace fine sand, wet - gray (CH) | 74 | 98- 96-46 | DH-T |
| Curve See Vane Shear | - | - | - | - | - | - | - | , | £ | Clay, trace fine sand, wet - gray (CH) | * | <u>94-</u> | DH-T |
| See Vane Shear | - | 1 | - | - | - | - | - | 1 | EI | Clay, trace fine sand, wet - gray (CH) | * | 89 | DH-T |
| yemsr,ka | Specific Specific | % Passing No.200 Sieve | Neturel Moisture (%) | 8 I4 | FF TWTC9 TGE | | Stratum Natural Density Desturation | | Deardna | Description of Soll Specimen | Sample | Elev. Depth | Boring No. |

3. Key to abbreviations: LL-Liquid Limit; PL-Plasticity Index.

PL=Plastic Limit; Fl=Plasticity Index.

+ 5. Visual description based on nearest jar sample.

Notes: 1. Soil tests in accordance with applicable ASTM Standards.

Soil classifications in accordance with Unified Soil Classification System.

SUMMARY OF SOIL LABORATORY TESTS

| | | | | | | | | | | | AND DESCRIPTION OF THE PERSON NAMED IN | - | |
|----------------------------|----------------------|-----------------------------|----------------------------|----|---------|-----|-------------------|-----|---------|---|--|-----------------|---------------|
| See Triaxial Test Curve | 2.65 | 46 | T.E8 | 99 | 33 | 88 | TS | 63 | ਬੁੰ | Clay, trace fine sand, with shell fragments—gray (CH) | əduT | 79- TL-69 | DH-2 |
| See Triaxial Test Curve | 2,65 | 00Т | 8.73 | 09 | 30 | 08 | 89 | 86 | В | Clay - gray (CH) | PoluT | 191-11 | DH-2 |
| CULVE See Vane Shear | - | - | - | - | - | | - | - | E | Clay, trace fine sand, wet- dark gray | H | 198-1/8 | ₽-HCI |
| See Vane Shear | - | - | - | - | - | - | | - | Я | Clay, trace | ** | 7S- 1T9-6S | ₽-HO |
| See Vane Shear | - | - | - | - | - | 1 | - | - | Я | Clay, trace fine sand, wet- dark gray (CH) | ** | 34-36 | ₽-HQ |
| See Triaxial Test Curve | 69°2 | 66 | 2.28 | 20 | 97 | 94 | ZS | 96 | я - | Clay, with gray (CH) | əqnL | 94- | DH-3 |
| See Triaxial Test Curve | 2.75 | 00Т | p.67 | 89 | 56 | 1/6 | ε\$ | 1/6 | . A | Стау-дкау (СН) | əqnL | 99-199 | £-Ha |
| нешықа | Specific Specific | gniaaay% 00%.oM sveis | Matural Motsture (%) | | terberg | | ral sity TC | Met | Designa | Description of Soil Specimen | Sample | Sample Depth | Boring No. |

3. Key to abbreviations: Leliatity Index.

Notes: 1. Soil tests in accordance with applicable ASTM Standards.

4. Soil Tests were conducted by B. Frey, L. Clark. * 5. Visual description based on nearest jar sample.

2. Soil classifications in accordance with Unified Soil Classification System.

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SUMMARY OF SOIL LABORATORY TESTS

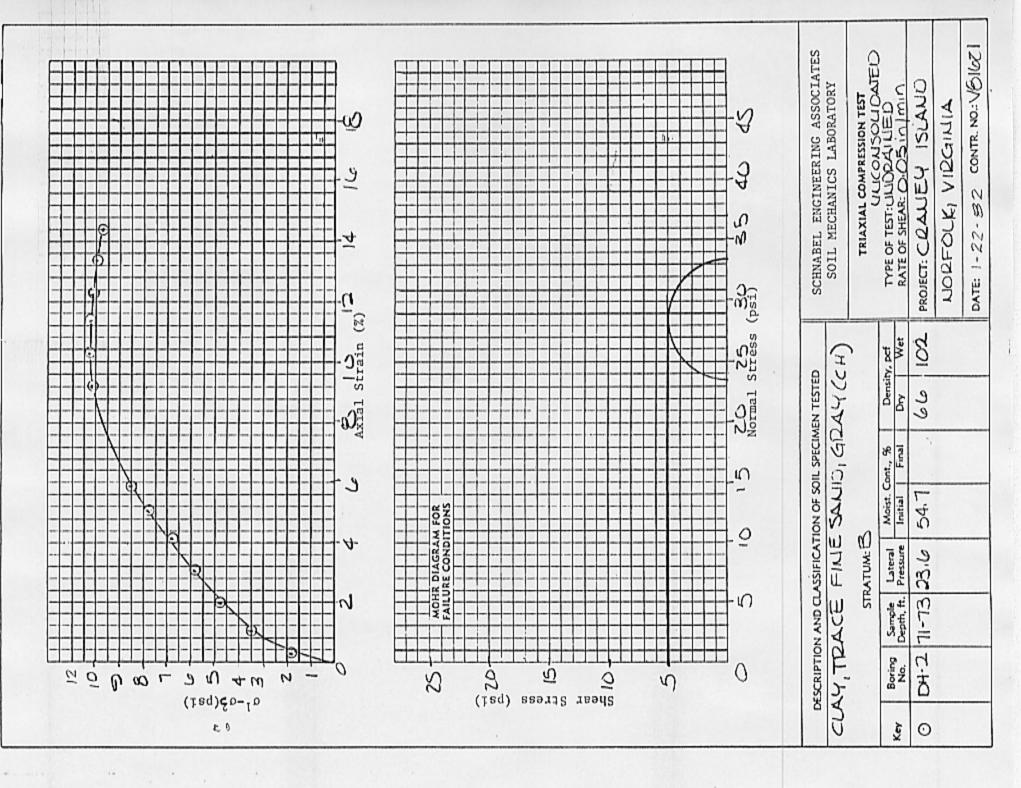
| CMLVE See Vane Shear | - | _ | | - | - | - | 1 | 1. | 3 | Fine sandy clay, wolst - dark gray (CL) | * | -95 100-105 | L-HO |
|----------------------------|---------------------|------------------------------|----------------------------|-----|------------------------|------|---------------------|--------------------|----------------------------|--|------------|------------------|---------------|
| Curve See Vane Shear | - | - | - | - | - | 1 | 1 | | E | Clay, trace fine sand, wet - gray (CH) | 5 + | 174-69 | ∠-Ha |
| CULTURE Shear | - | - | - | - | - | 1 | 1 | - | В | Clay, trace fine sand, wet - gray (CH) | × | 6E- 19\$-\$\$ | L-HQ |
| See Triaxial Test Curve | 89.2 | 00Т | 2.69 | 81/ | 52 | · LL | 89 | 66 | B | Clay, with shell fragments - gray (CH) | eduT | £6- ,T0T-66 | DH-6 |
| See Triaxial Test . | £7.2 | 66 | 0.18 | £9 | 30 | 83 | 25 | ∌ 6 | Я | Clay - gray (CH) | eduT | -73-67 | DH-6 |
| See Triaxial Test Curve | 17.2 | 96 | 9 .1 9 | 34 | εħ | LL | £9 | EOT | В | Clay, trace fine sand, with shell fragments - gray (CH) | Tube | 34-361 | DH-6 |
| See Triaxial Test Curve | 07.2 | 00Т | 7.SA | TS | 55 | ₽8 | 99 | ₽6 | В | Clay, trace fine sand - gray (CH) | PduT | 198-18 | DH-2 |
| gewarks | Gravity Specific | Z Passing No.200 Sieve | Metural Moisture (%) | | br tmtts terberg | | red Stry Stry | Natu Den Wet | Stratum Designa tion | Description of Soil Specimen | Sample | Elev. Depth | Boring No. |

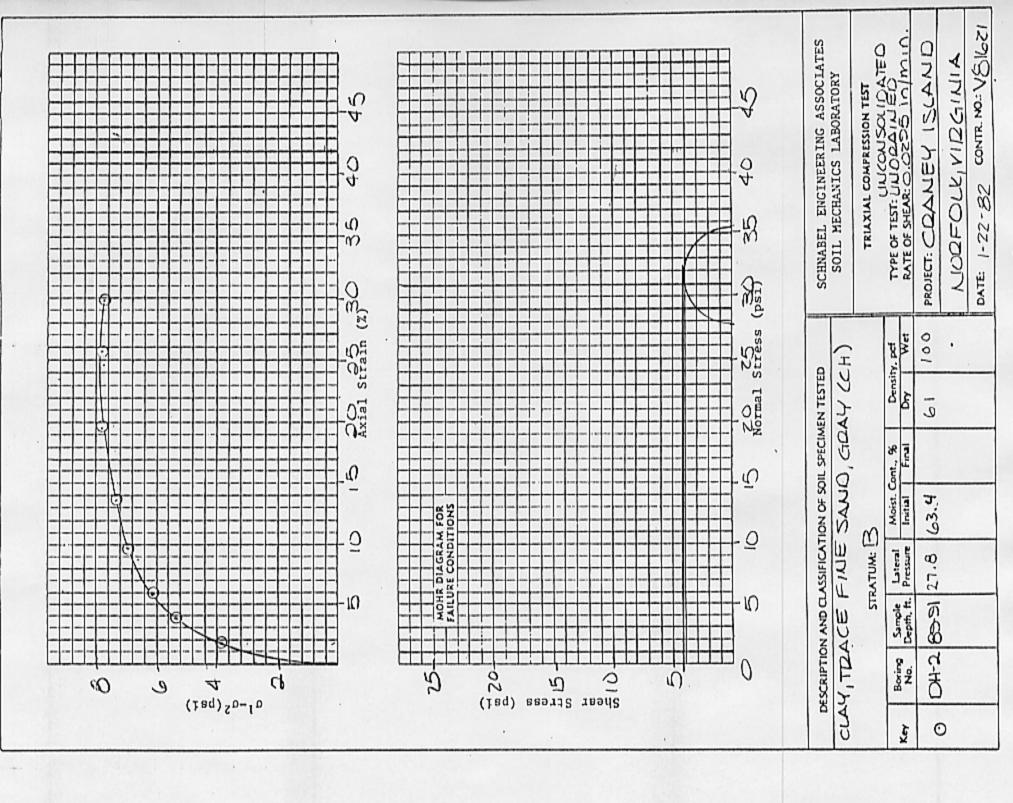
3. Key to abbreviations: LL-Liatity Index.

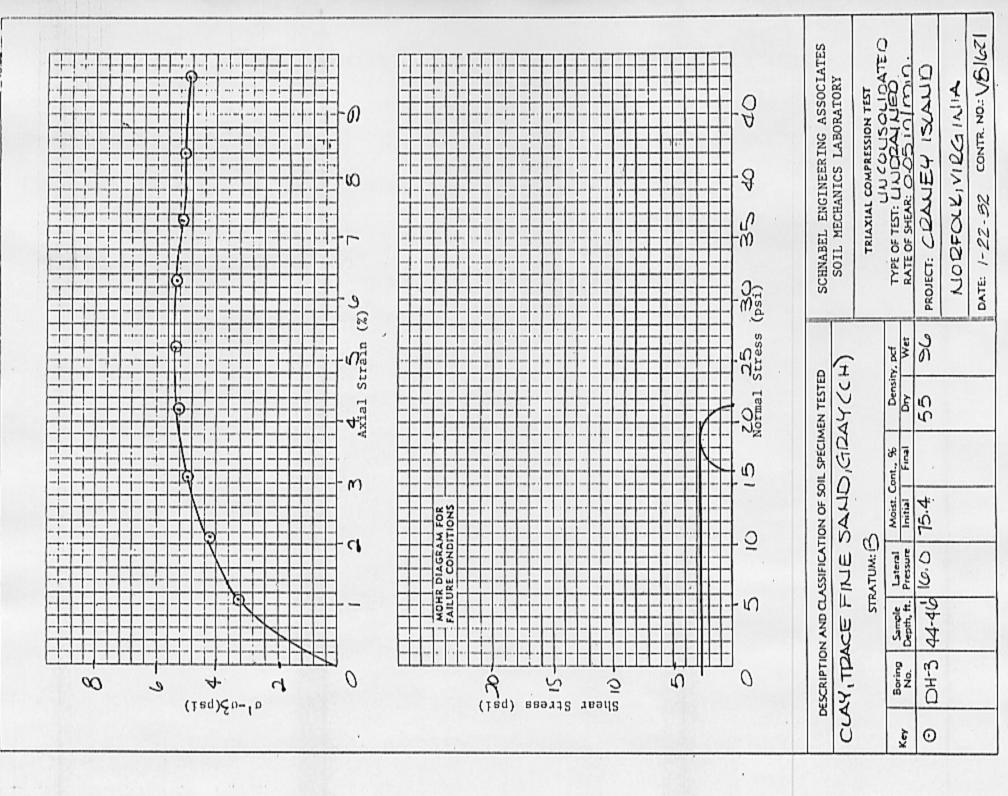
4. Soil Tests were conducted by B. Frey, L. Clark.

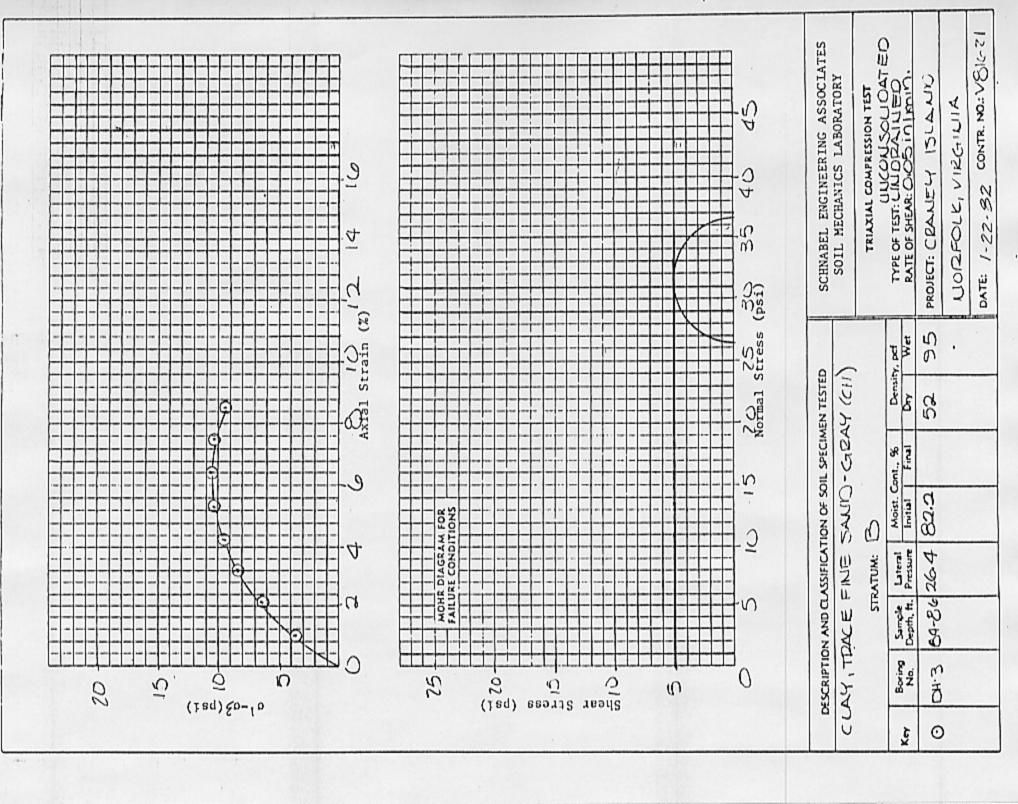
Notes: 1. Soil tests in accordance with applicable ASTM Standards.

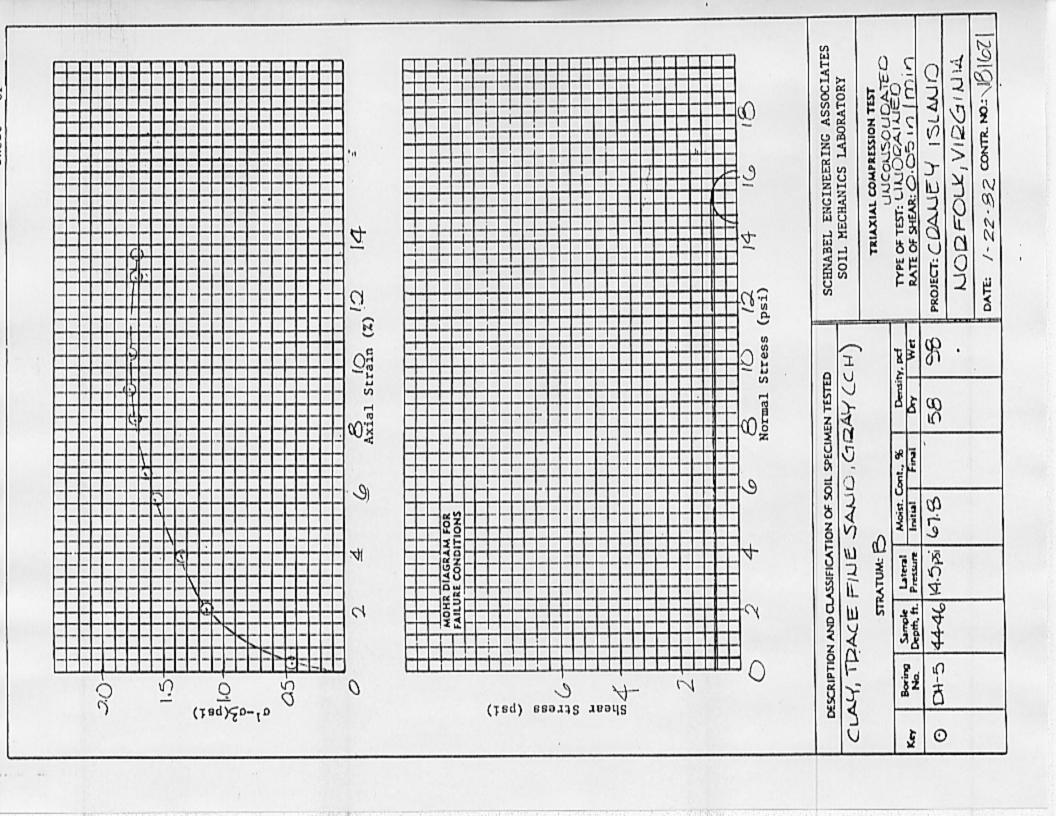
 Soil classifications in accordance with Unified Soil Classification System.

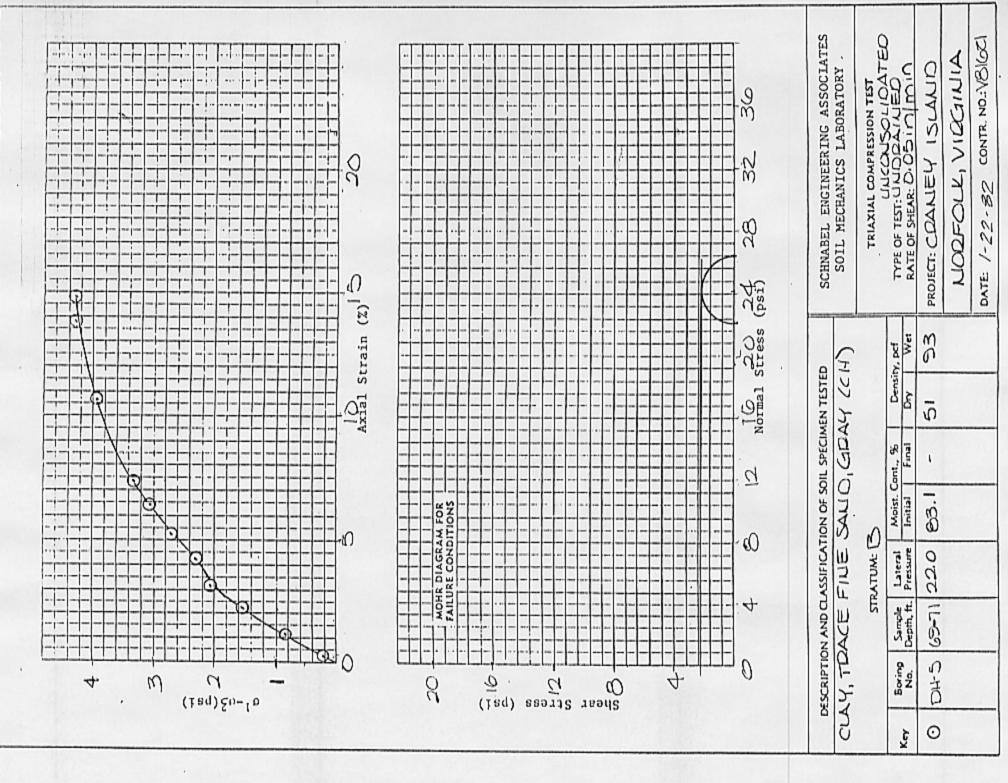


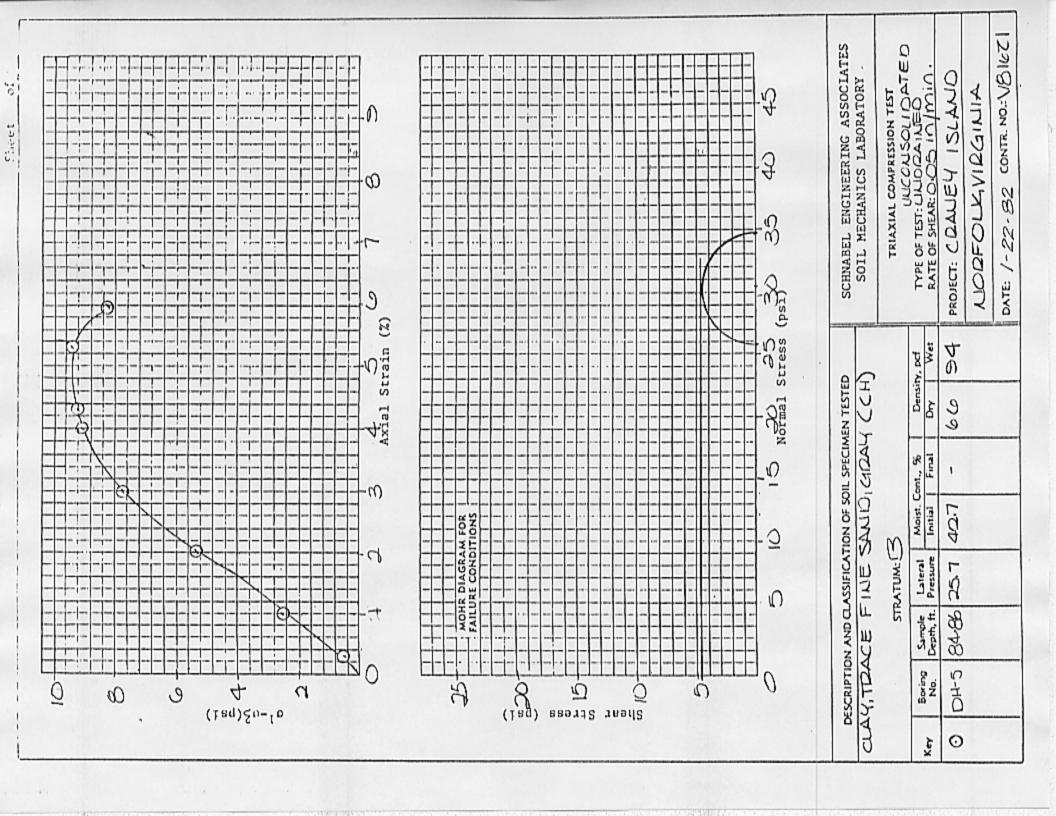


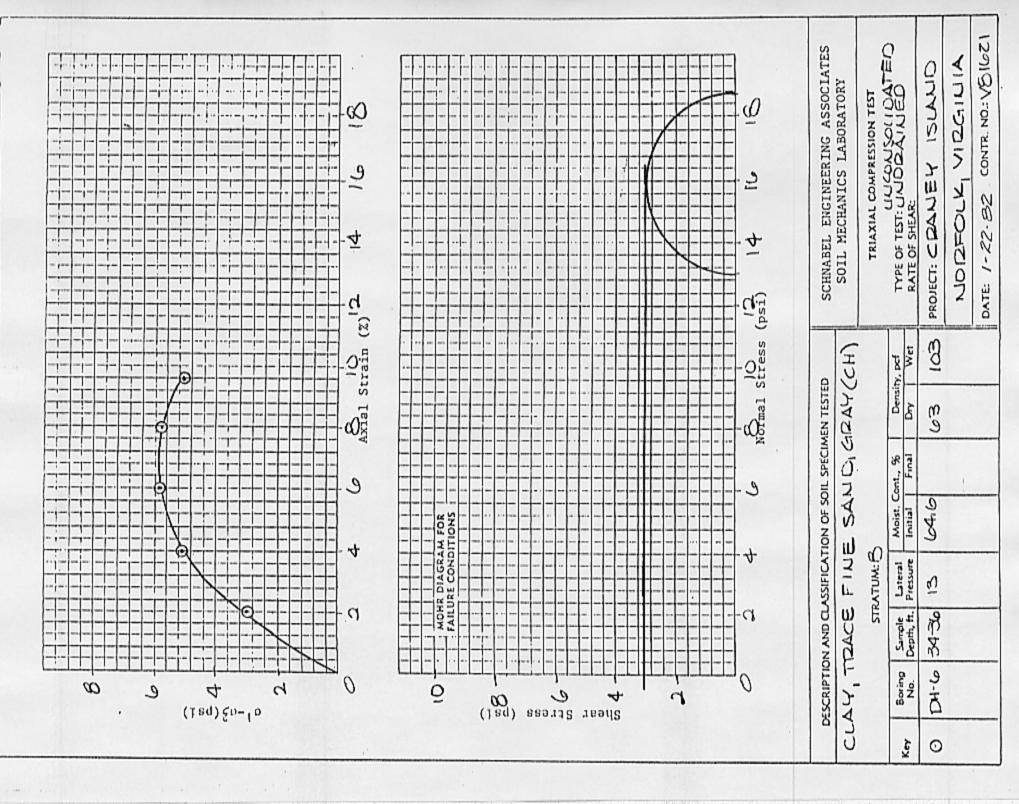


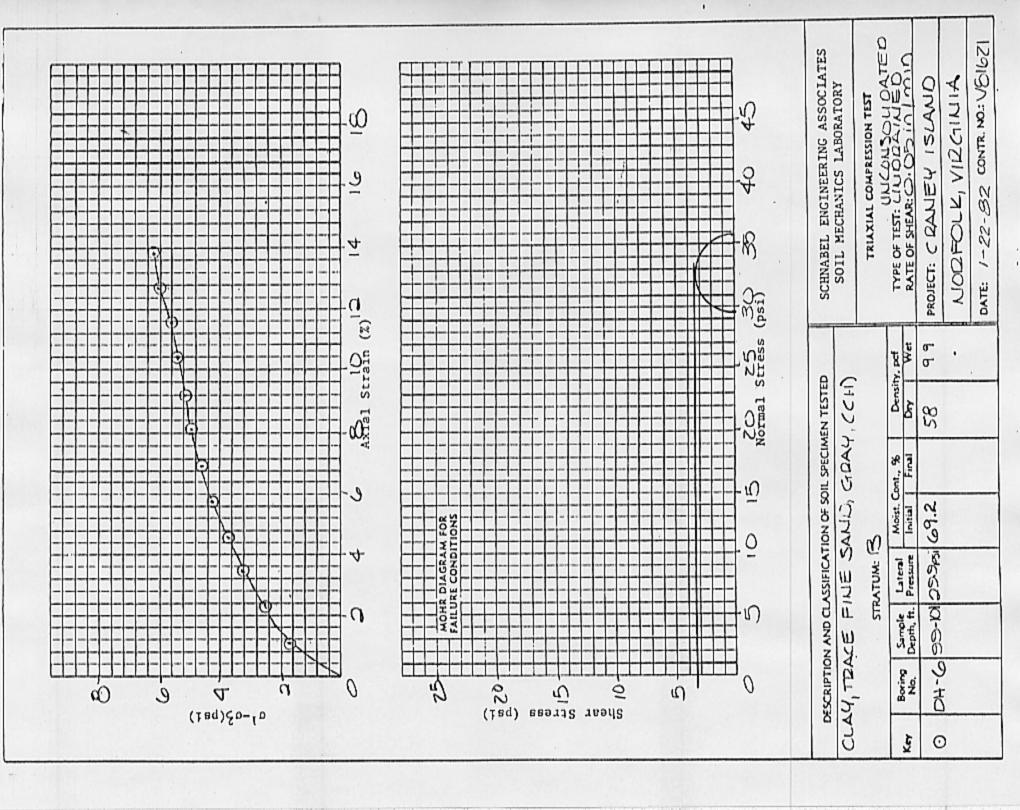


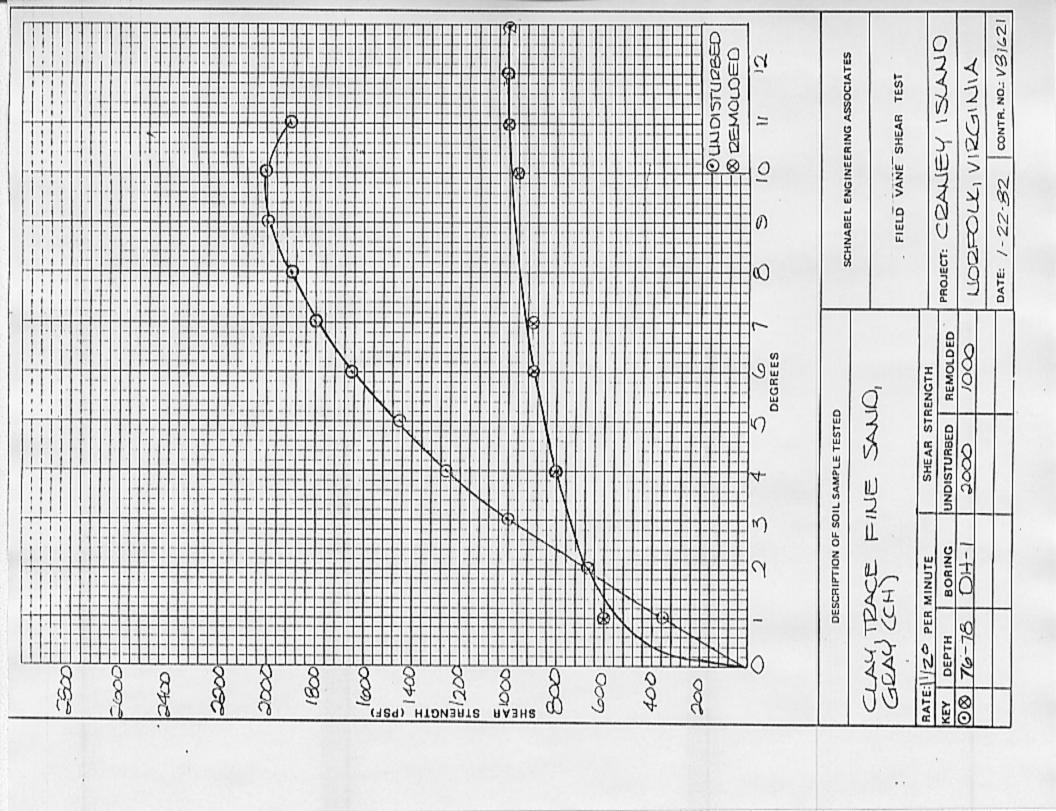


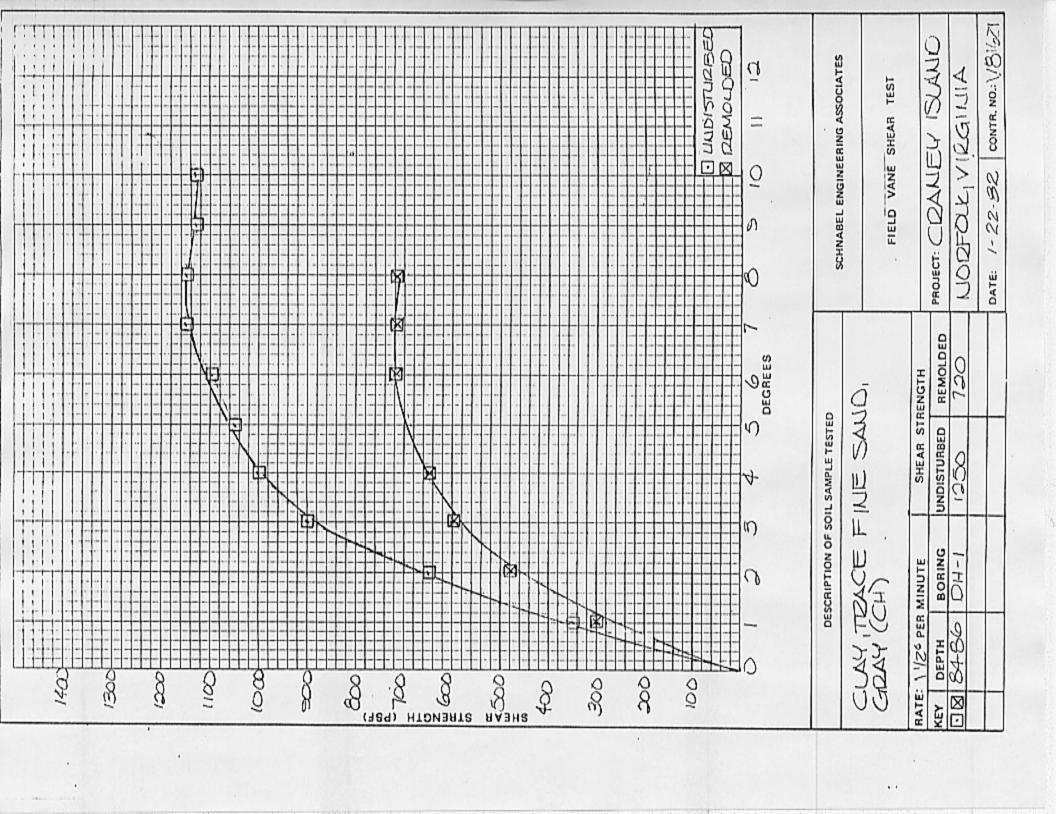


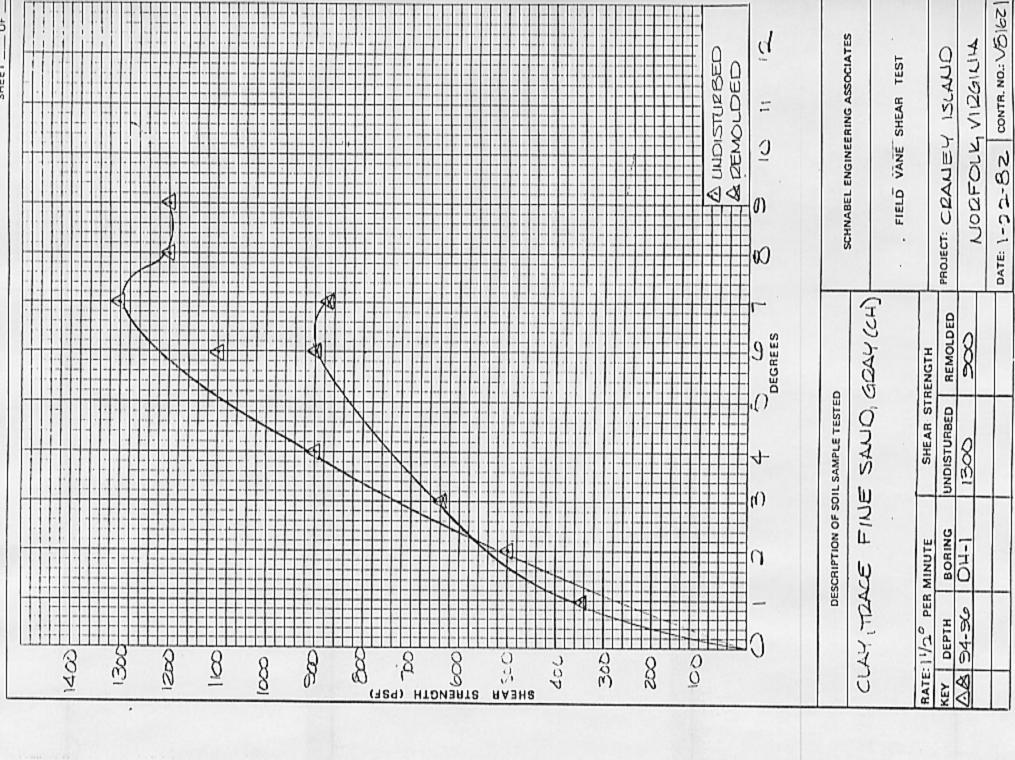


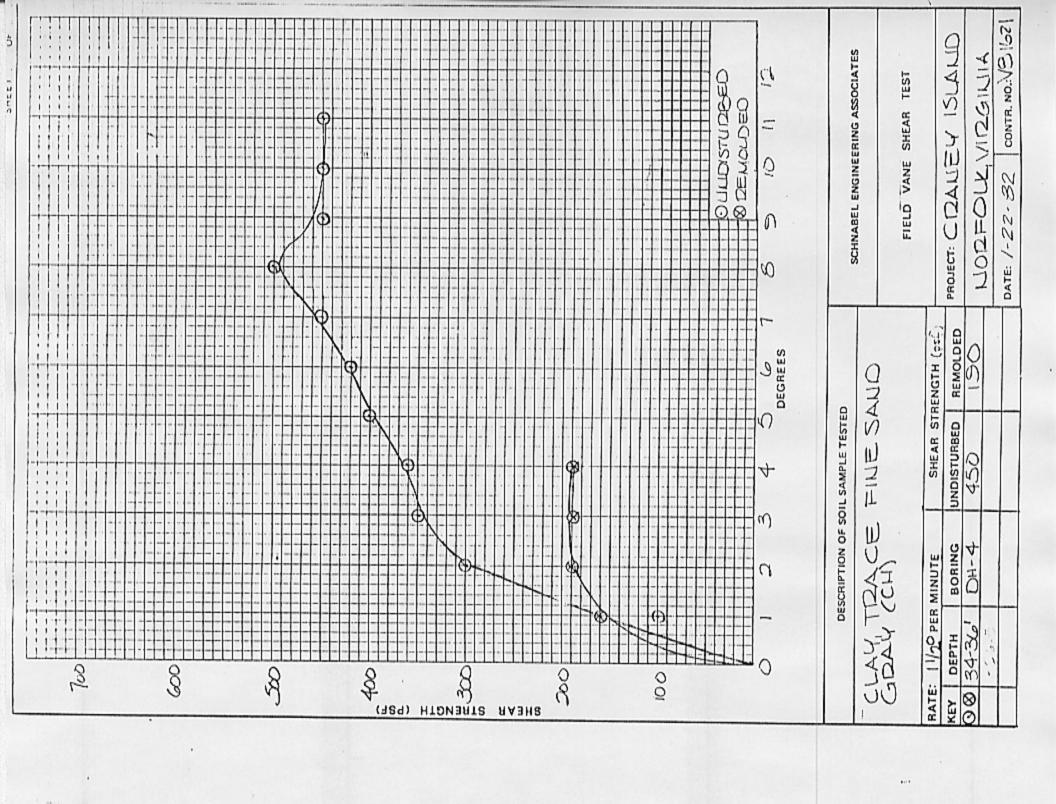


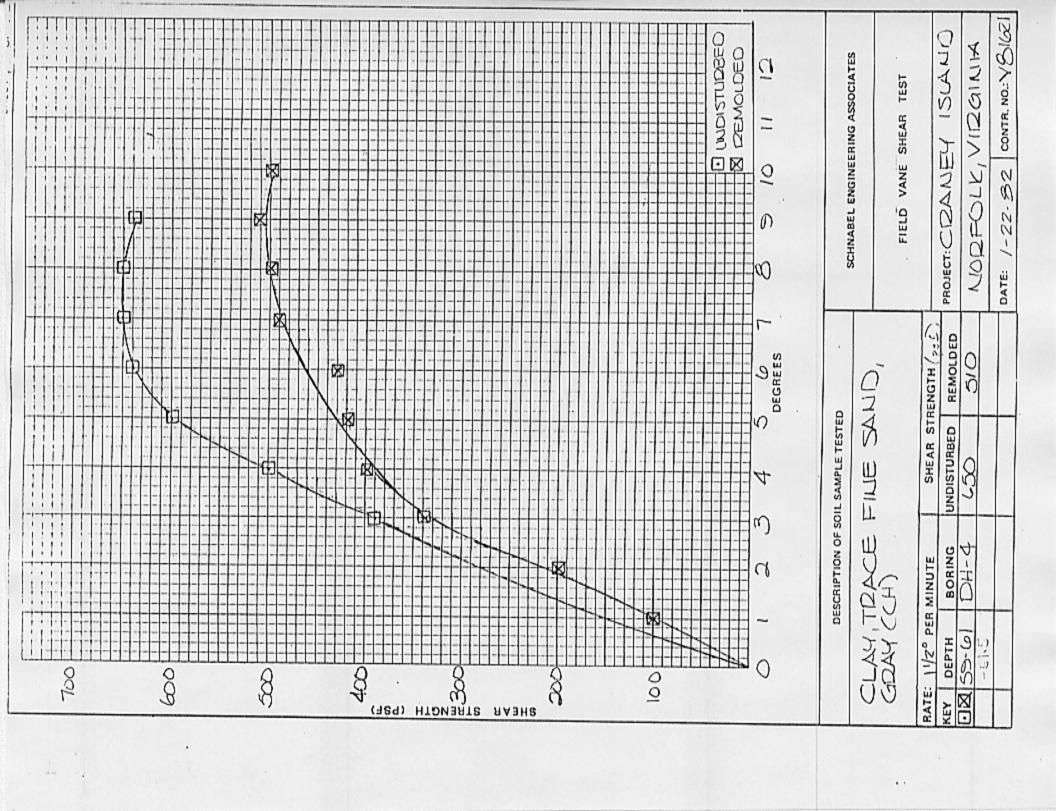


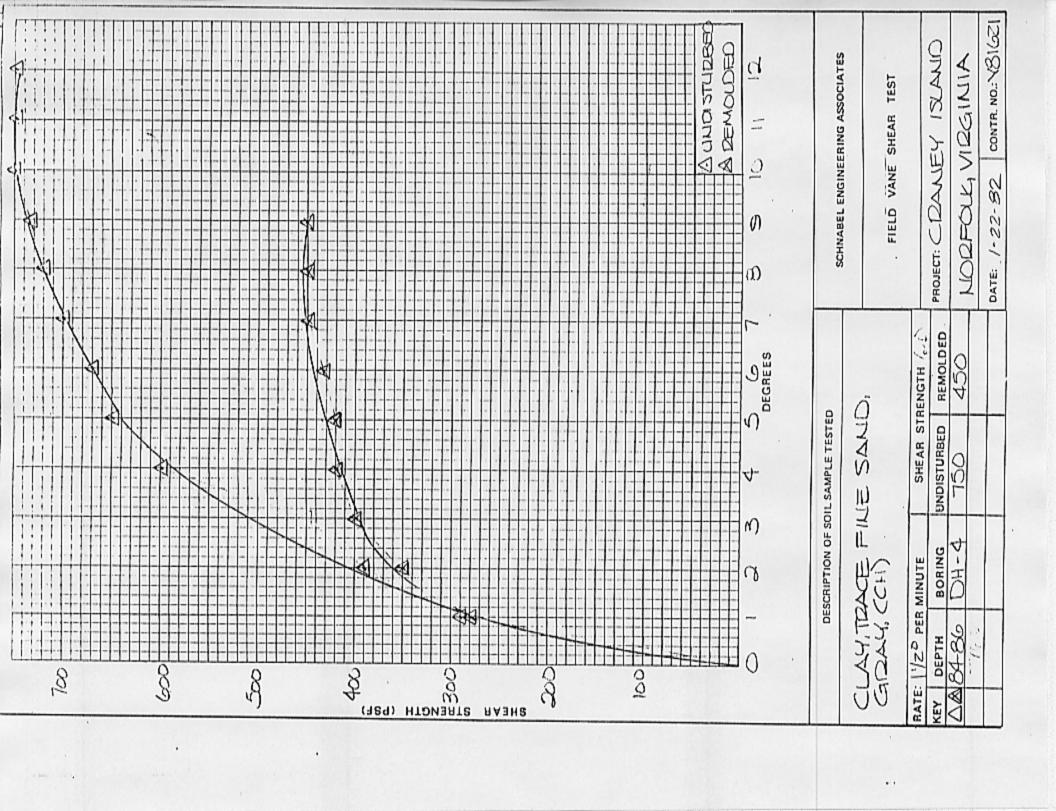


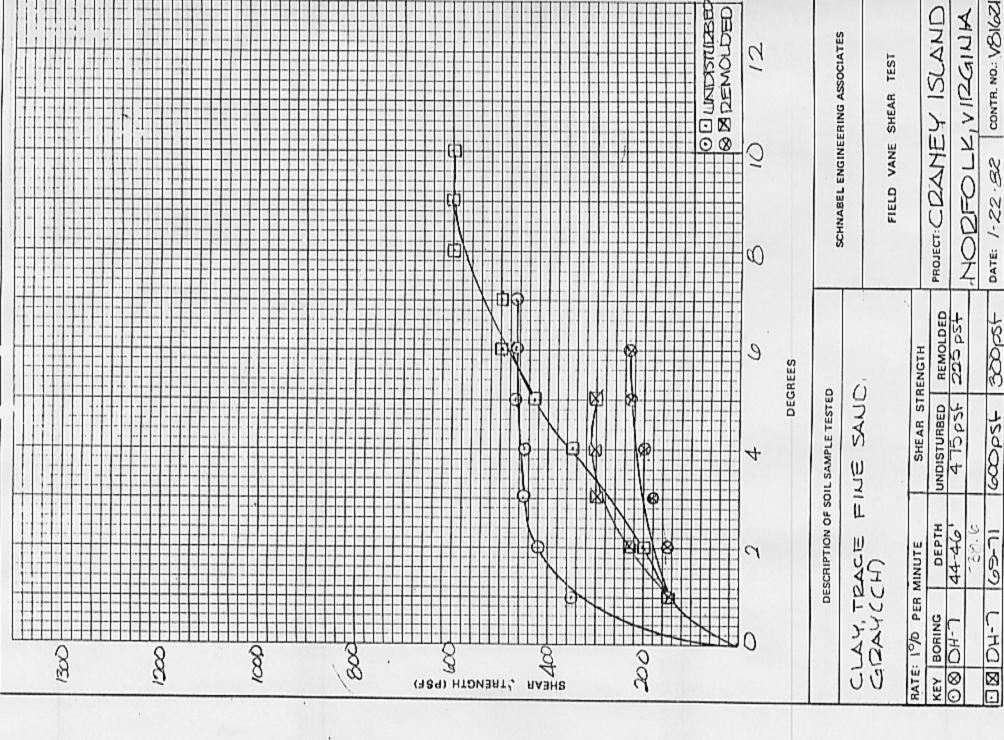




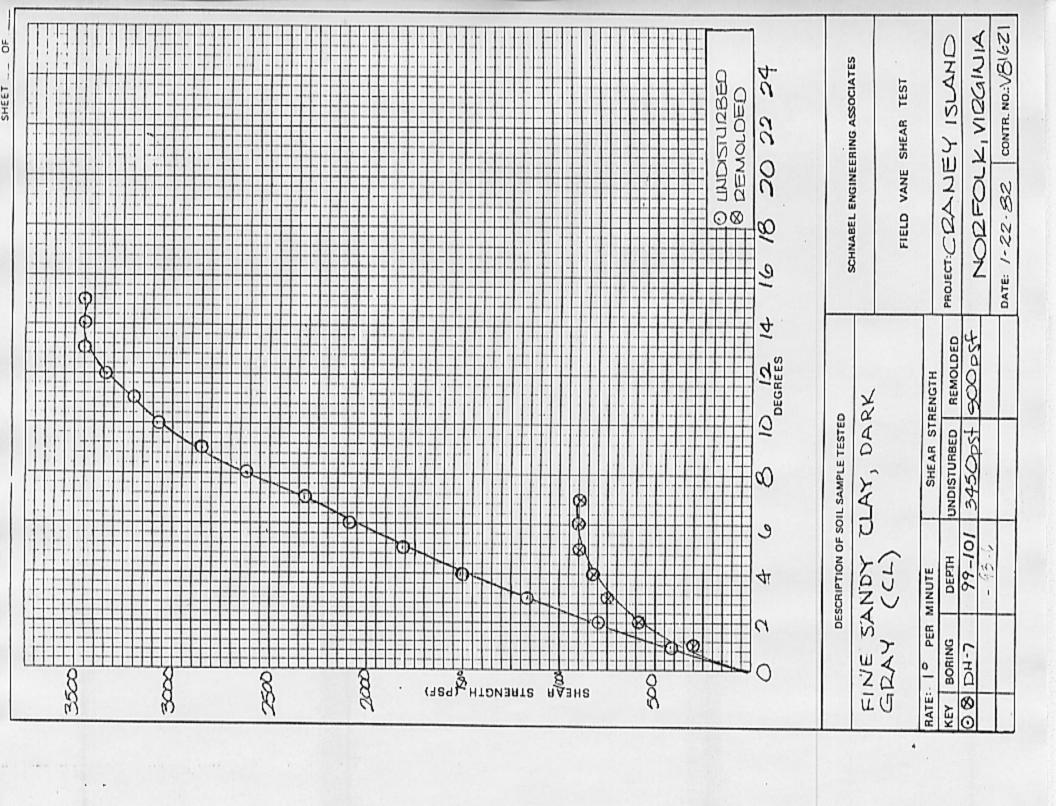








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SUBSURFACE EXPLORATION DATA

General Notes for Test Boring Logs
Identification of Soil Samples
Test Boring Logs, DH-1 through DH-7
General Site Location Plan, Sheet 1
Estimated Subsurface Profile, Sheet 2

Test Borings

Standard Penetration Test (SPT) was performed at the depths indicated depth with plug inserted. The SPT was performed following removal The The augers were advanced to the desired All borings were drilled by hollow stem auger equipment. of the plug. Water level data is indicated on the logs. on the Test Boring Logs.

Boring Location and Elevation Survey

Test boring elevations were estimated based on a topographic survey of the site dated April, 1980, provided to us by the Corps of Test borings were located in the field by Corps of Engineers personnel. Engineers

GENERAL NOTES FOR TEST BORING LOGS

- 0.D., 1-3/8 INCH I.D. SAMPLING SPOON 6 INCHES USING A 140 POUND HAMMER FALLING NUMBERS IN "SAMPLE SPOON" COLUMN INDICATE BLOWS REQUIRED TO DRIVE A 2 INCH 30 INCHES ACCORDING TO ASTM D-1586. i
- SHOWN IN FORTH SET THE UNIFIED SOIL CLASSIFICATION SYMBOLS TERMINOLOGY SOIL IS IN ACCORDANCE WITH PARENTHESES ARE BASED ON VISUAL INSPECTION. "IDENTIFICATION OF SOIL." VISUAL CLASSIFICATION OF 5
- THESE LEVELS ARE ONLY ESTIMATES ESTIMATED GROUNDWATER LEVELS INDICATED BY ; THESE LEVELS ARE ONLY ESTIMATES FROM AVAILABLE DATA AND MAY VARY WITH PRECIPITATION, POROSITY OF THE SOIL, SITE ESTIMATED GROUNDWATER LEVELS INDICATED BY TOPOGRAPHY, ETC. ë
- REFUSAL AT THE SURFACE OF ROCK, BOULDER, OR OBSTRUCTION IS DEFINED AS PENETRATION RESISTANCE OF 100 BLOWS FOR 2 INCHES PENETRATION OR LESS. 4
- THE BORING LOGS AND RELATED INFORMATION DEPICT SUBSURFACE CONDITIONS ONLY AT THE SOIL CONDITIONS AT OTHER LOCATIONS MAY DIFFER FROM CONDITIONS OCCURRING AT THESE BORING LOCATIONS. ALSO, THE PASSAGE OF TIME MAY RESULT IN A CHANGE IN THE SUBSURFACE SOIL AND SPECIFIC LOCATIONS AND AT THE PARTICULAR TIME WHEN DRILLED. GROUNDWATER CONDITIONS AT THESE BORING LOCATIONS. 5
- SOME VARIATION THE SOIL PROFILE, WATER HAVE BEEN MADE WITH REASONABLE CARE AND ACCURACY AND MUST BE CONSIDERED ONLY AN LEVEL OBSERVATIONS AND PENETRATION RESISTANCES PRESENTED ON THESE BORING LOGS THE STRATIFICATION LINES REPRESENT THE APPROXIMATE BOUNDARY BETWEEN SOIL AND APPROXIMATE REPRESENTATION OF SUBSURFACE CONDITIONS TO BE ENCOUNTERED AT THE ROCK TYPES AS DETERMINED FROM THE DRILLING AND SAMPLING OPERATION. MAY ALSO BE EXPECTED VERTICALLY BETWEEN SAMPLES TAKEN. PARTICULAR LOCATION. ė,
- BORING LOG VERTICAL SCALE: 1/10 INCH = 1 FT. 7.
- , RICHMOND, VIRGINIA UNDER INSPECTION OF SCHNABEL ENGINEERING ASSOCIATES. TEST BORINGS DRILLED BY AYERS AND AYERS, INC. 8
- KEY TO SYMBOLS AND ABBREVIATIONS: 6

| NO SAMPLE RECOVERY | do, DITTO | RQD, ROCK QUALITY DESIGNATION | NATURAL MOISTURE CONTENT | | | | |
|-----------------------------|-------------------------------------|------------------------------------|--------------------------|-------------------|--------------------------------|------------------------------------|---|
| * | do, | RQD, | 'n | | | | |
| S STANDARD PENETRATION TEST | 2" 2" or 3" UNDISTURBED TUBE SAMPLE | (RECOVERY SHOWN IN REMARKS COLUMN) | PRESSUREMETER TEST | V VANE SHEAR TEST | C STATIC CONE PENETRATION TEST | (RECOVERY SHOWN IN REMARKS COLUMN) | I |

SCHNABEL ENGINEERING ASSOCIATES Consulting Geotechnical Engineers

IDENTIFICATION OF SOIL

| T PROPERTIES | Approximate Percentage by Weight | 50 or more | 35 to 50 | | 12 to 35 | 1 to 12 | indicates | presence | | |
|--|-------------------------------------|---|---|-----------------|----------------------------------|--------------------------------|-----------------|----------------------------|--|--|
| II. DEFINITION OF COMPONENT PROPERTIES | Proportions of Soil Components | Noun Form Gravel, Sand, Silt, Clay, etc. | Adjective Form Gravelly, Sandy, Silty, Clayey Silty, Clayey, Silty Clayey | | Some Gravel, Some Silt, etc. | Trace Gravel, trace sand, etc. | With | with organic matter. | | |
| 11. | Component | Major | Minor | | | | | | | |
| NENTS | Plasticity | 11 | | Non-plastic | Slight to High | Medium to High | Very High | Slight to High | c matter with or with | |
| I. DEFINITION OF SOIL COMPONENTS | Sieve Size | 3/4 to 3" No. 4 to 3/4 | No. 10 to No. 4 No. 40 to No. 10 No. 200 to No. 40 | Passing No. 200 | Passing No. 200 | Passing No. 200 | Passing No. 200 | Passing No. 200 | Partially decomposed fibrous organic matter with or with out silt or sand filter | |
| I. DEFINIT | Material Fraction | Coarse Fine | Coarse Medium Fine | 1 | 1 | - | 1 | 1 | Partially dec out silt or sar | |
| | Major Material Component | GRAVEL, GM, GC, GP, GW | SAND, SM, Coarse SC, SP, SW Medium Fine | SILT, ML | CLAYEY SILT, ML, MH, CL-ML | SILTY CLAY, CL | CLAY, CH | ORGANIC SILT, OH, OL | PEAT, PÉ | |

III. GLOSSARY OF MISCELLANEOUS TERMS

SYMBOLS - Unified Soil Classification Symbols are shown in major material component column. Use A Line Chart for laboratory identification.

BOULDERS - Rounded pieces of rock larger than 3 inches

DISINTEGRATED ROCK - Residual soil with a standard penetration resistance of at least 60 blows or more per foot

ROCK FRAGMENTS — Angular pieces of rock, distinguished from transported gravel, which have separated from original vein or strata and are present in a soil matrix.

QUARTZ - A hard silica mineral often found in residual soils

IRONITE - Iron oxide deposited within a soil layer forming camented deposits

CEMENTED SAND - Usually localized rock-like deposits within a soil stratum composed of sand grains cemented by calcium carbonate or other minerals

MICA — A soft silica mineral found in many rocks, and in residual or transported soils derived therefrom

FISSURED CLAYS - Cohesive soils exhibiting a joint structure

ORGANIC MATERIAL (Excluding Peat): Top Soil — Surface soils that support plant life and which contain considerable amounts of organic matter; Decomposed Vegetation — Partially decomposed organic matter which retains its original character; Lignite — Decomposed organic matter with low fixed carbon content frequently exhibiting distinct texture of wood

FILL - Man made deposit containing soil, rock and often foreign matter

PROBABLE FILL - Soils which contain no visually detectable foreign matter but which are suspect with respect to origin

LENSES - 0 to 1/2 inch layer of minor soil component

LAYERS - 1/2 to 12 inch layers of minor soil component

POCKEI - Discontinuous pocket of minor soil component

MOISTURE CONDITIONS - Wet, moist, or dry to indicate visual appearance of specimen COLOR SHADES - Light or dark to indicate substantial differences in color

| BORING NO.: D8-1 SPEET NO. 1 OF 2 JOB NO. V 91621 ELEMATION: 8.81 CASING SIZE: 28- DATE FINISHED: 1-5-82 DRILLER: N. ANDES INSPECTOR: G. ADAYS | REMARKS | | | ii. | , | | |
|--|----------------|---|-------------------------|--|---------------------------------------|--|---|
| NG LOG ND, NORECLX RELL: CSE-55 RINE SAMPLER TYPE S.S. TYPE S.S. TYPE S.S. TYPE SAMPLER TYPE SAM | IDENTIFICATION | FINE TO COMPEE SAND FILL, TRACE SILL, MTH SHELL FRACEDIES, MDIST - TAN (SP) do, NET | FRANKIS, NET - GEIN (SQ | FIRE TO CONSEE SNO FILL, TRATE SILL, WER CONV. (SP.) OO, FIRE TO MENIN SNO, TRACE SILLY CLAY WANTCHOOLD | 6, fire to coase sad, trace sult, day | FRE SILK SND FILL, ART - GRY (SN) | FIRE TO ORSEE SNO FILL, TRACE SILT, WITH SHELL FRANCENS, NET - GRAY (SP) |
| SCHMABEL ENGINEERING ASSOCIATES TEST BORI CONSULTING ENGINEERS STUDY, CHARGIT ISLA CLUENT CHARGITA MICHAEL DATA BORNE, CHARGITA MICHAEL DATA BORNE, DATA WATER LEVEL DATA CHARGITA MICHAEL DATA CASING PULLEDIL-5 3:334 DRC 1.5' WATER CASING PULLEDIL-5 ASSOCIATION OF PRINCIPLE READING BACKITL URCH CASPIETTION IS | MUTANTA | 34444 10+16+17 0 6+444 | 44647 8 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | A | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 54.0 7+12+14 S 4+3+13 S |

| NO. DH-1 | SHEET NO 2 OF 2 CORNO VELSCOLO CHATCALO ET | REMARKS | TILL | Su = 2000 psf | Su = 1250 psf. MARDE CLAY | S _{tr} = 1300 psf | , | |
|---------------------------------|--|---|---|---|------------------------------|----------------------------|-----|------------------------------|
| MTES TEST BORING LOG BORING NO. | Y, CHAEY ISLAMD, MORGER IX, VINGINGA | D ANTES INC. | FIRE TO COASE SAD, TRCE SILL, WET - CAN (SP) FIRE SAD, SOVE CLAIR SILL, WET - GRAY (SA) | CLAY, TRACE FIRE SND, NET - DATA GRAY (CN) | | \$ \tag{8} | | BORING TEMPROTED AT 105.0 FT |
| SCHABEL ENGNEERING ASSOCIATES | PROJECT WEST LEVEE ALLIGNEST OF IENT CORPS OF ENCHOSISS. | A TOOMAN ON THE HILD CONTRACT | 3147(4)[| 74.0 (2+2+2 S | > vs v | | ğ ğ | |

| BORING NO.: DH-2 SHEET NO. 1 OF 2 JOB NO.: V81621 ELEVATION: 6,812 CASING SIZE: 347 DATE START: 12/2/81 DATE FINNELD: 12/2/81 DATELER: C. JANZESCH INSPECTOR: J. MOSIDHI | REMARKS | • | | | TIL. | | | Tube pressed 24" Recovery = 0" | Tube Pressed 24" - Recovery = 24" | | | |
|---|---|--|--------------------------|--|----------|---|--------|-----------------------------------|---|---------------------------------------|---|--|
| TEST BORING LOG OY, CRAEY ISLAND, MIROLK S., INC. DRIVE, SAMPLER S., INC. DRIVE, SAMPLER EPTH CAVED TYPE S.S. EPTH CAVED TYPE S.S. ON 1 - 01A. 2.00 S. 01.0' WT. 190* | IDENTIFICATION | FINE TO COASE SHO FILL TRUC SILT WITH SPELL TRUCKINS, MOIST - TRN (SP) do, NET | do, fire snd, ket - Gray | ENE, MIST - DAM GAV (CH) TO MIST - DAM GAV (CH) TO MISTA SAO FILL, TACE SI | AL. | פא. דוסב עס מאפסב פאוט, אבד - ידאו אוט מאצ | | | FIRE TO COMPER SHIP, SOME SHIPN CAN WITH SHIPL FRANCE/S, MOIST - CAN (SC) can (SC) ch, interested Can | do, with fire game. | | FIRE TO COMPRE SAND FILL, TRACE SILT HER - BRORN (SP) do, BRORN NEJ GRAY |
| HUBEL ENGINEERING ASS CONSULTING ENGINEE DECT MEST LIVE ALIG ENGINEERING MERS WATER LEVEL DONTERED (27/23 TER CASING PULLED/27/24 DY READING (17/24) | STRATON STRATON THE SECON THE | | 2+3+3 \$ | , | \$ 5+++2 | 20 1+9+7 5 | (+9+8) | 3+3+5 | \$ E | 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | 1 | (a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c |

| BORING NO. DE-2 | No. 2 OF 2 | JOB NO.: V81621 | REMARKS | THE . | | Tube Pressed 24* Recovery = 24* | | | MATTE CLAY | | | | Secovery = 18" | | | | | · | | | | | | 1 |
|--|------------|--|--------------------------------------|---|----------------------------|------------------------------------|-------|----|--------------|----|----|---|-------------------------------------|---------|---|----------------|---|----|---------------------------------------|---|---|------|---|---|
| BORIN | SHEET | 308 W | | D FILL, | GRAY (CH) | | | | | | | | 83 | | | | | | | | | | | |
| ATES TEST BORING LOG | | DE, NOROUX, VINCINGA AND AVES. INC. | | ARCH ALL GRAY FIRE TO COARSE SAND TRACE SILT, NET - BROAN (SP) | CAY, THE PIE SNO, NOST - G | do, Sell magers | | | do, past day | | | | ès, no fine sano or seell finandars | | | | | | POSTING OFFICE CONTRACTOR OF THE OPEN | | | | | |
| SOCI | GNE | | TOBMAS | 1 | 'n | :1 | S | | U) | (n | T | 1 | 5 5 | | | l _s | Г | 1. | | | | - | | _ |
| BEL ENGINEERING ASSOCIATES CONSULTING ENGINEERS | LEVEE ALI | CLIENT, CORPS OF ENGINEERS, | SHOUNS SAMPLE SPOON 12 P.31 | | 1+2+3 | | XDR+2 | | WOR | 25 | | T | WOR ! | | | ACR. | | | | | | | | |
| ENGIN | VEST | CHE | 'AZTZ | -60 | 0 | | -12 | 25 | 6/2 | 7 | 99 | | * | | 8 | | | | | | | | | Ī |
| SCHWABEL | PROJECT: | CLIENT: | HI 130 | A 67.0 | Щ | Ш | Ц | Ц | П | | | П | Ш | \prod | Ţ | Ц | Ι | | | Ц | I | Ц | П | Ι |
| | | | | 103/ | | | | | | | | | | | | 33.5 | | | 100 | | | | | |

| BORING NO.: DE-3 SPEET NO. 1 OF 2 JOB NO. VRIGH. ELEWION: 8.62 CASING SIZE: 3%* DATE START: 12/24/81 DATE START: 12/24/81 DATE START: 12/26/81 DATE START: 12/26/81 | REMARKS | Ė | | | | MADE CLAY The Presset 24" Recovery = 24" | | Tube Pressed 24* Recovery = 24* |
|---|----------------|---|-----|----------|--|---|------------|------------------------------------|
| CONSULTING ENGINEERS TEST BORING LOG | IDENTIFICATION | | ### | 29.0 -20 | 1+1+1 S CAY, TRACE FIRE SAND HITH SHELL FRACEATS, MOIST - DARK CRAY (CR) | B | -40 MORE S | -50 MOR S |

| BORING NO. DE-3 | NO. 207 2 .: V81621 | REMARKS | | PREDICT CLAY | Tube pressed 24* Recovery = 24* | | 1 | |
|---|--|---|--|--------------|------------------------------------|-------------------|--|-------------------------------|
| TEST BORING LOG | VT STITY, CHANTY IS AND WINSON K SHEET NO. 2 WYSOLY VINCINIA 108 NO.: VB | IDENTIFICATION | CLAY, TRACE FINE SAID WITH SHELL FRACENTS, MIST - DAN GRAY (CH) | | 9 5 | o, in sect months | SILT CAY, THE SAD WIN MCA NO HOD, HOLT - DAR CAY (C.) | BORDAG TERMINAND AND 100.0 FT |
| SSOCI | 388 | TOUMAS | 0 0 0 | u) | in w | u u | us | |
| SCHNABEL ENGINEERING ASSOCIATES CONSULTING ENGINEERS | PROJECT: NEST LEATE ALLGOSOF STITY CLERT: CORPS OF ENGINEERS MOONE 308 PMC CHESTATOR: ALLGO AND ALERS. | SEGON SEGON SYMILE ON BLOWS | MOR MOR | 88 | . 808 | WOR | MCR+1+4 | |
| ENG | CORP | EPEA" | 5 9 C | -70 | 8 | 4 . 9 | 8 | |
| SCHNABEL CON | CLIENT: | H1430 | | ЩШ | Ш | 0.0 | 1000 | |
| | | | | m | | | 15 | ' |

| BORING NO. DE-4 SHEET NO. 1 OF 2 LOB NO. 381-51 ELEMINON: 81-52 DATE STAFT: 1-4-82 DATE FINISHED: 1-4-82 DRILLER: NAMES INSPECTOR C. ADMS REMARKS | TILA | Su = 450 paf | NAD CAN | Su = 540 psf |
|--|--|---|---------|--------------|
| SCHNABEL ENGNEERING ASSOCIATES TEST BORING LOG CONSULTING ENGNEERS FROLECT NEST LEVER ALLOMENT STUDY, CHMEN ISLAND, NORFOLK, VIGINAL OCCUPANTION STUDY, CHMEN ISLAND, NORFOLK, VIGINAL OCCUPANTION STUDY, NORFOLK, VIGINAL OCCUPANTION STUDY OF THE SAMPLER CASING SIZE. BORING CONTRACTOR NORFOLK ALROYED TYPE S.S. BATE START: BOROWITCHER CASING PULLED A 4.40 DRY 1.2' WT. 140 ** DRIVE FINISHED MATERIAL OCCUPANTION STUDY OF THE FINISHED MATERIAL OCCUPANTION STUDY OF THE FINISHED MATERIAL OCCUPANTION STUDY OF THE FINISHED MATERIAL OCCUPANTION STUDY OCCUPANTION STUDY OCCUPANTION STUDY OCCUPANTION OCCUPANTIO | \$ 5 8 5 8 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 9 6 | 23.0 -20 1+1+1 S CLAY, TSACE FINE SAND, HET - INHIS GRAY (CH) | S | S |

| BORING NO.: DE-4 | CNO. 2 OF 2 | TON: 8 ST | REMARKS | | MADE | Su = 750 psf | | | 1. | |
|---|--|------------------|---------------------|--|-------|--------------|-------|-----------------------------------|-----------------------------|--|
| SCHABEL ENGNEEPING ASSOCIATES TEST BORING LOG BORING CONSULTING ENGINEERS | ALIGNOS STUN, CHARY ISLAM, NORDIK SHEET NO CONTESS, NORDIK, VIRGINIA | 24 3 | POST OF THE CATION | S CAY, THATE FIRE SWD, WET - DAWN GRAY | S S | | v1 v1 | CLAY, TRACE FINE SMO, WITH CRIMIC | BORDIG TENDROED AT 100.0 FT | |
| SCHWBEL ENGNEES CONSULTING E | CLIENT CORS OF PICKETS, NORTH | BORNG CONTRACTOR | ELEY FL BLOWS | \$ C | -7- B | 08- | 2 S | -90 | | |

| BORING NO.: DH-5 SHEET NO.: OF 2 JOB NO.: V81521 ELEMETON: 7.34 CASING SIZE: 34 DATE STAFF 12/28/81 ORILLER: R. ANESS INSPECTOR: J. K81281 | HEMARKS | a a | | 112 | | | מזא | Tube Pressed 24* Personary = 24* | |
|--|--|-------------------------------|--|-----------------------------|--|---|-----|--|--|
| C. E. | 7.5t d case 2 Fire to coarse samp fill, mace sin | WITH SELL FRACENTS, POIST - G | 8+15+17 S do, FINE TO MEDINA - GAV-CREEN 4+1+4 S | 1-21-6 5 do, SNE SILT - GNV | 1+1+1 S CAN, SOME PIDE SNO WITH SHELL -20 PROPERTS, MOIST - DAN GRAF (CL.) | WORT S CLAY, TRACE FIRE SND WITH SEEL. FRACEUTS, MIST - DUR. CRAY (CI) | -30 | 40 WORN S WO FIRE SND OR SHELL FRANCENTS WOR S SHELL FRANCENTS | |
| SCHOUGH COLIENT COLIENT BYTER CE 24 HR. F. | | | 4 | | 39.0 | Ш | t t | | |

| BORING NO. DE-5 | NO. 2 OF 2 | ET EVALION: 7.91 | REMARKS | Tibe Pressed 24" Recovery = 24" | CLAN . Dube Pressed 24* Peacovery = 24* | | |
|--|-------------------------------|--------------------------------------|---|------------------------------------|---|---------------------------------------|-------------------------------|
| BORII | SHEET. | EVA. | | ٠ | | | |
| TEST BORING LOG | P. STEDY, CRACK IS NO. NORDIX | MARING CONTACTOR: AVES NO AVES. D.C. | IDENTIFICATION | Can, the sub him sell. | CO, 10 SELL FRANCIS | | BORING TERMINATED AT 100.0 PT |
| ASSOCIA | MIGNER | 1 | TORMAS . | - N N | 0 5 0 0 | N N N N N N N N N N N N N N N N N N N | |
| BEL ENGINEERING ASSOCIATES COMSULTING ENGINEERS | EVER AL | DR: AV | BEN 9. SENDON SENDE ON DECOMS | # E | NOR NOR | 25 S | |
| NSULTIN | T TEST | 100 | Elev. | 8 2 6 | 8 | 8 | |
| SCHWABEL | PROJECT: NEST LEVES | DETAC C | H1430 | | | | |

| S S | | | | i | |
|--|---|--|--|----------------------------|---|
| BORING NO.: DH-6 SHEET NO.! OF 2 JOB NO.: VALLO.! ELEVATION. 7.01 CASING SIZE: 34* DATE START: 12/35/81 DATE FINSHED: 12/35/81 DATE FINSHED: 12/35/81 INSPECTOR: 3. AVESS INSPECTOR: 3. AVESS INSPECTOR: 3. AVESS INSPECTOR: 3. AVESS | | Į. | Tube Pressed 24** Recovery = 24** | MADE CAN | |
| BORING SHEET NO ELEVATION CASING SI DATE STA DATE FIN INSPECTOR | LEDS WITH SOLD INCOME. | | | Ĭ. | |
| CATES TEST BORING LOG NE STUDY, CHANCY ISLAND, NORDLK NAME OF THE SAMPLER ME DEPTH CAVED TYPE S.S. ME DEPTH CAVED TYPE | FING TO COMPES SHO, SOVE SILE WIT FINGERS NO GAMEL, MOIST - DW do, TSMCS SILE, WET do, FINE, Wet - GAW-GREN | के, 1962 SILT, NET - GAN | CLV, TSACT THE SAND WITH SEEL FRACENS, NOIST - GRY (CI) | غە, <u>1540 - 1700 (مە</u> | do, GNV |
| SCHMABEL ENGINEERING ASSOCIATES TEST BORIL | 1, 7+13+13 1, 7+13+13 0, 7+19+23 1, 1+18+25 1, 8+9+18 | 10 10 10 10 10 10 10 10 10 10 10 10 10 1 | 23.0 -20 11-1-1 S 1-1-1 S 1-1-1 S 1-1-1 S 1-1-1 S 1-1-1 S 1-1-1 S | 65 140 80 | -50 H-22 S-22 H-23 S-23 S-24 S-24 S-24 S-24 S-24 S-24 S-24 S-24 |
| | | | 5 | | |

| BORING NO. 24-6 SEEET NO. 2 OF 2 JOB NO. 1 VELSO ELEVATION: 7.05 REMARKS | Tube Pressed 24" Recovery = 24" . MAINE | The Pressed 24" Recovery = 24" | | |
|--|--|---------------------------------------|--|-----------------------------|
| CRAEN ISLAND, NORMEN INC. VIRGINIA INC. INC. INC. INC. INC. INC. INC. INC. | מאי , זאתב דותב פאנט, אמופך - מפבא- מאי (מו) מי, אט פאדנו דאמפטונט, מאיצ | do, hin sell fradens | à, soe fde sho fde Clave sho, mist - Dar Gew (SC) | BORDES TEMPORED AT 115.0 PT |
| SCHALBEL ENGINEERING ASSOCIATES TE CONSULTING ENGINEERS SLUDY, CLIBAT MESST IEVES MIGNERS NO MISSOCIATES NO MISSOCIATE NO MISSOCIATES NO MISSOCIATES NO MISSOCIATES NO MISS | -60 NOR S S S S S S S S S S S S S S S S S S S | S S S S S S S S S S S S S S S S S S S | 111.00 S | |

| SOWWERLEDGE PARKETHO ASSOCIATES TEST BORING LOG | BORING NO.: DB-7 SHEET NO. 1 OF 1 JOB NO. VB162) CLENATION: 6.42 CLASNG SIZE: 2% DATE STATE: L230/81 DATE FINISHED: 1/5/82 DRILLER: R. AYENS INSPECTOR: J. MOSLEH | REMARKS | TILA | | | MANDE CLAY Su = 475 pet | |
|---|--|--|--|---|---|-------------------------------|----|
| | NG LOG JAD , NOFFOLK RILL: OST-55 RIVE SAMPLER RIVE SA | SAMBOL SVANE E SVANE BLOWS SELLEY SEL | (+1)+15 S FIRE TO COLVEE SAD, TRACE SILE V 12+12+17 S SHPLI FRACEATS, MOIST - TRA (SR O 9+11+13 S do, NET O 9+11+13 S do, FIRE SAD D O 2+7+12 S NET - TRA (SR) | 210 316-11 S FIRE TO COMPERS SWED, TRACE SILL 20 SHELL FRACEDITS, NET - CRAY (SP) | 1-1-1 S CLN, TRACE FDE SNO NTH SELL (CON (CON (CON (CON (CON (CON (CON (CON | HOR S | 20 |

| TEST BORING LOG BORING NO. 12 STUTY, CHART ISLAND, NORDIK SHELT NO. 2 OF 2 |
|--|
| 7150,013 |
| IDENTIFICATION |
| 8 |
| THAS FIRE SND, MOIST - DARK GREEN (CH) |
| |
| |
| |
| do, with Sell Francis |
| |
| |
| |
| |
| 2,5 |
| באסי כבעי, אסובד - נאפו נפוע (כב) &נ |
| |
| MODIN SWD, TRACE CLAY, GRY (SC) SOC |
| FIRE SANDY CLAY, ATM NOD FRACEITS, MOST - DARK CRAY (CL.) |
| |
| FIRE TO NEITH SWD, TRATE STIF, WET - NUMBER TO NEW TOWNS ONLY CREEK (SM) |
| בה 115.0 בה מבהשתמשבה מתחפת |
| |

-110 18 3 -20 ė 18 0 80 70 8 105' LEOW <u>a 0 88 5</u> õ Ū (J) Ö 6 5 N MALAGES W02 ξu most 105' 1,000 eB Ü 00 ő e 07-7 a OW STRATUM SCALE: 1' = 400' 0 10 ξø 600 200 Elop 4 ĘZ ō O ő 520 30 STRATUM 400 800 HOZIZ. 888 200 200 BB BB 200 8 4 822 84 0 3 w +100 W. C. C. STDATUM "A" SECTION A.A E E FIGS+ 100. 203 EUD 2000 203 283 FEBRU 500 ESS. 82828 a O STRATUM 6 WOR 203 200 888 188 mo2 CUCE 200 model M324115' wee ERR 2000 79 33 Ø n STEATUM WOR STDATUM 13 20'EI 2000 489 wice 20m was 2000 2000 WOD. 8 3 288 4E V STRATUM C" -10 8 B 8 18 ġ 6 8 0 7.

SENERAL NOTES

NUMBERS TO THE LEFT OF THE BORING COLUMNS INDICATE NUMBER OF BUT TO DRIVE A 2 INCH O.D., 1-3/8 INCH I.D. SAMPLING SPROW ONE FOO

10

GS EL 8.8 GS EL 68

92 EL 66

05EL65

GSEL 7.9

GSEL 7.0

GSEL 64

ó

140 POUND HAVER FALLING 30 INCHES, ACCORDING TO ASIM D-1586.

6. S. - GROUND SUBFACE

WOR - WEIGHT OF RODS

NO UNDESTURBED TO

TEST BORINGS DRILLED BY AYERS AND AYERS, INC. IN DECEMBER 1981 JANUARY 1982.

THESE PROFILES WERE DEVELOPED BY INTERPOLATION BETWEEN WIDELY S
ONLY AT THE BORING LOCATIONS SHOULD THEY BE CONSIDERED AN AN AS
ACCURATE REPRESENTATIVE AND THEN ONLY TO THE DEGREE IMPLIED BY THIS IMAMING CONTAINS INTERPRETATION OF TEST ECRING DATA AND SUSED AS PART OF THE CONTRACT DOCUMENTS.

TEST BORINGS INSPECTED BY SCHWBEL ENGINEERING ASSOCIATES. THE BORING LOGS.

LOCATIONS AS SHOWN ON SHEET 1. STRATA DESCRIPTIONS

STRATUM A: TAM, BROWN OR GRAY FINE TO COARSE SAND FILL WITH VARIAGE \overline{B}^2 SILT AND CLAY (SP, SM AND SC); (N = 3 to 50) STRATUM E. DARK GRAY FINE SANCY CLAY WITH WOOD FRACHENTS (CL) AND STRATUM-BE GRAY CLAY, TRACE FINE SAND WITH SHELL FRAGMENTS (CHI); MEDIUM SAND, TRACE CLAY (SC); (N = NOR TO 6)

STRATUNDS: BRAY-GREEN FINE TO MEDIUM SAND, TRACE SILT (SM); (N -Eclose

SCHNABEL ENGINEERING A

STIMATED PENER ADDITION COM NODERLY VIDGINIA

PROFILES SUBSUDFACE OPO. 13 8 10

Ō, SO VERT

